

## Fingerite, $\text{Cu}_{11}\text{O}_2(\text{VO}_4)_6$ , a new vanadium sublimate from Izalco volcano, El Salvador: crystal structure

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### Abstract

Fingerite,  $\text{Cu}_{11}\text{O}_2(\text{VO}_4)_6$ , is triclinic with  $a = 8.1576(6)$ ,  $b = 8.2691(5)$ ,  $c = 8.0437(7)\text{\AA}$ ,  $\alpha = 107.144(5)^\circ$ ,  $\beta = 91.389(7)^\circ$ ,  $\gamma = 105.441(5)^\circ$ ,  $Z = 1$ , and space group  $P\bar{1}$ . The crystal structure has been solved and refined to a weighted  $R$  of 0.044 from 2875 intensities measured on a four-circle diffractometer. The structure consists of vanadium in tetrahedral coordination and copper in octahedral and trigonal bipyramidal coordination with Jahn-Teller distortions typical for  $\text{Cu}^{2+}$ . The octahedra form a sheet with holes and are cross-linked by vanadium tetrahedra and copper trigonal bipyramids.

### Introduction

Fingerite,  $\text{Cu}_{11}\text{O}_2(\text{VO}_4)_6$ , a fumarolic mineral from Izalco volcano, El Salvador, is described in the preceding paper (Hughes and Hadidiacos, 1985). It is a double honor to have the mineral named after me and to have the opportunity to solve and present its crystal structure.

### Experimental

A crystal of fingerite,  $0.09 \times 0.09 \times 0.15$  mm, was mounted on a four-circle diffractometer, and the orientation matrix and reduced unit cell were determined by an automatic indexing algorithm similar to that suggested by Jacobson (1976). The cell proposed by Hughes and Hadidiacos (1985) was confirmed. In the final orientation the axis of crystal rotation was approximately parallel to  $[3\bar{8}2]$ . Unit-cell and orientation parameters were refined from the positions of 20 independent observations with  $39^\circ \leq 2\theta \leq 54^\circ$  measured by the eight-reflection centering method of King and Finger (1979). The unit cell and other crystal data are listed in Table 1.

The intensity data for one hemisphere ( $l \geq 0$ ) of the triclinic mineral were measured to  $60^\circ 2\theta$  with omega step scans and Nb-filtered Mo radiation. The resulting data were integrated by application of the Lehmann and Larsen (1974) technique for optimum background selection. In accordance with the suggestions of Gabc (1980), the inner edge of the background region was selected two steps outside the point corresponding to the minimum in  $\sigma/I$ . Integrated intensities were corrected for Lorentz-polarization and absorption effects ( $\mu_1 = 143.2 \text{ cm}^{-1}$ ) with the program of Burnham (1966). A total of 2875 intensities were measured. Of these, 2257 had values greater than twice the standard deviation.

Solution of the crystal structure was accomplished through use of the tangent formula as implemented in MULTAN-80 and associated programs (Main et al., 1980). Pseudosymmetry of the copper and vanadium atoms resulted in some difficulty in the solution (cf. Hai-Fu et al., 1983). In addition, the formula as derived from electron microprobe analyses was thought to be  $\text{Cu}_{10}\text{V}_6\text{O}_{25}$ . Despite these difficulties, successive cycles of

Fourier syntheses revealed the positions of all atoms, the correct stoichiometry and confirmation of the space group ( $P\bar{1}$ ).

Program RFINE4 (Finger and Prince, 1975) was used to refine the structure. Effective standard deviations,  $\sigma'$ , used to calculate least-squares weights, were calculated from the formula  $\sigma'^2 = \sigma^2 + (0.012F)^2$ , where  $\sigma$  is the standard deviation derived from counting statistics and  $F$  is the structure factor. All structure-factor calculations were performed with neutral atom scattering curves selected from the data of Cromer and Mann (1968). Anomalous dispersion coefficients were taken from *International Tables for X-Ray Crystallography, Vol. IV* (1974). The refined structure converged to an  $R$  factor of 7.6% with isotropic temperature factors and an isotropic secondary extinction coefficient. After conversion to anisotropic temperature factors, the structure converged to a weighted  $R$  of 4.4% and an unweighted  $R$  of 4.6%. The anisotropic refinement is significantly better than the isotropic calculation (Hamilton, 1965). Robust/resistant techniques (Prince, 1982) were employed in the final stages of the refinement. Final observed and calculated structure factors are listed in Table 2.<sup>1</sup> Refined atomic coordinates and equivalent isotropic temperature factors are listed in Table 3.

### Description of the structure

The anion arrangement of  $\text{Cu}_{11}\text{O}_2(\text{VO}_4)_6$  may be described as essentially a close-packed array of oxygen. Octahedrally coordinated copper ions form a sheet with holes (Fig. 1). These edge-shared polyhedra have Jahn-Teller distortion typical for  $\text{Cu}^{2+}$  (Shannon and Calvo, 1973). Each octahedron has four equatorial oxygen ions at distances approximately equal to  $2\text{\AA}$  (Table 4) and two apical oxygens at greater distances. For Cu3 and Cu4, the

<sup>1</sup> To receive a copy of Table 2, order Document AM-85-258 from the Business Office, Mineralogical Society of America, 2000 Florida Avenue, N.W., Washington, D. C. 20009. Please remit \$5.00 in advance for the microfiche.







5	707	719	632	626	115*	145	125	247	210	940	976	1377	1370	308	374
6	482	499	2	145	147	460	464	341	335	1951	1519	347	357	350	374
7	253	255	3	284	460	171	188	27*	89	486	462	240	225	624	647
8	117*	71	H 10	0	171	289	138	735	765	1447	1382	598	581	243	291
9	327	293			219	138	138	491	521	224	232	118*	108	178	200
					197	138	138	882	979	398	339	603	624	1467	1473
					1079	1067	1067	374	370	653	650	200	169	258	251
					2012	2033	2033	200	195	695	694	108*	20	79*	20
					626	667	667	82*	34	547	567	87*	12	216	213
					144	150	183	131	119	61*	71	108*	57	929	907
					203	236	236	157	116	285	289	87*	57	336	347
					256	14	14	131	119	26*	43	H -8	2	614	618
					657	643	643	157	116	427	415	29*	11	1092	1097
					88*	143	143	492	483	307	302	506	556	30*	34
					641	648	648	753	748	427	415	179	175	171	180
					30*	83	83	560	519	280	325	625	672	286	233
					H 11	0	0	365	338	170	168	127*	159	390	379
					154	116	116	658	627	100*	8	1204	1220	H -2	2
					985	985	985	479	464	479	464	82*	54	563	528
					327	317	317	577	579	307	302	27*	36	161	180
					427	414	414	1262	1194	427	415	179	175	525	476
					890	863	863	30*	45	28*	22	94*	92	1132	1123
					218	219	219	883	908	607	578	721	747	310	348
					444	441	441	239	256	48*	22	25*	102	453	514
					978	975	975	820	897	259	256	326	294	113	113
					461	460	460	445	466	190	180	180	168	839	887
					230	253	253	446	464	265	223	H -7	2	163	166
					115	100	100	446	464	265	223	H -7	2	123	95
					H 5	0	0	761	718	H 7	1	182	219	149	134
					194	211	211	108*	1381	330	323	101*	81	120	116
					152	132	132	162	142	269	281	276	284	198	149
					522	527	527	254	268	254	268	519	504	29*	55
					913	940	940	276	274	100*	62	188	176	93*	50
					130*	89	89	108*	78	100*	62	0	188	909	909
					460	485	485	276	274	29*	15	585	598	926	909
					176	181	181	276	274	184	208	914	931	233	215
					453	485	485	276	274	385	394	103*	76	614	602
					351	367	367	458	423	542	509	409	397	28*	26
					581	584	584	458	423	168	157	402	401	H -1	2
					1387	1331	1331	458	423	1069	1024	520	543	432	86
					501	495	495	126*	131	967	930	444	455	86*	86
					229	244	244	126*	131	987	928	115*	86	432	395
					608	587	587	126*	131	987	928	115*	86	432	395
					246	246	246	126*	131	987	928	115*	86	432	395
					434	430	430	126*	131	987	928	115*	86	432	395
					dd*	106	106	126*	131	987	928	115*	86	432	395
					163	501	501	126*	131	987	928	115*	86	432	395
					952	951	951	126*	131	987	928	115*	86	432	395
					158	198	198	126*	131	987	928	115*	86	432	395
					890	888	888	126*	131	987	928	115*	86	432	395

Fingerite after Cycle 26

FACTOR = 10.00

Fingerite after Cycle 26

FACTOR = 10.00

H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC
-8	133	76	-6	563	582	-2	97*	166	-9	672	665	-11	30*	52	-8	326	334
-7	526	519	-5	516	532	-1	228	225	-8	428	419	-10	776	732	-7	82*	94
-6	83*	84	-4	295	305	0	405	434	-5	29*	108	-9	87*	108	-6	221	212
-5	1187	1208	-3	140	125	1	166	165	-4	83*	47	-8	29*	58	-5	260	247
-4	1032	1054	-2	143	97	2	161	92	-3	91*	67	-7	91*	67	-4	447	468
-3	134	115	-1	372	374	3	113*	68	-6	399	395	-6	389	418	-3	850	835
-2	1158	1232	0	850	791	4	467	474	-5	715	721	-5	715	721	-2	451	433
-1	435	470	1	2422	2342	5	51*	59	-4	291	322	-4	291	322	-1	723	718
0	467	463	2	100*	42	6	39*	10	-3	49*	77	-3	49*	77	0	59*	23
1	122	108	3	362	358	7	245	245	-2	114*	70	-2	320	294	1	525	510
2	1653	1666	4	105*	90	8	29*	37	-1	101	73	-1	101	73	2	71*	132
3	251	247	5	248	246	H-9	H-9	3	-6	680	710	-2	320	294	3	143	127
4	267	281	6	696	720	-4	96*	40	-7	114*	70	-3	49*	77	0	59*	23
5	932	917	7	357	335	-3	534	557	-8	28*	117	-4	291	322	1	525	510
6	80*	68	8	161	155	-2	531	553	-9	114*	70	-5	715	721	2	71*	132
7	102*	34	H 5	2	2	-1	326	346	-6	680	710	-6	389	418	3	143	127
8	172	203	-10	309	277	0	326	322	-5	497	535	-7	91*	67	4	413	396
9	239	244	-9	312	321	1	282	322	-4	150	180	-8	291	322	5	246	259
10	191	223	-11	658	625	2	282	322	-3	1005	1029	-9	101*	48	6	989	974
H 0	2	2	-8	28*	54	3	153	145	-2	175	132	-10	126*	32	7	386	373
-11	356	344	-7	580	586	4	297	308	-1	774	730	-9	743	739	-6	230	227
-10	139	116	-6	170	204	5	1089	1053	0	125	96	-8	840	835	-5	253	250
-9	432	425	-5	125	141	6	100*	11	6	890	871	-7	556	583	-4	212	167
-8	348	361	-4	241	217	7	710	690	7	362	369	-3	409	433	-3	392	391
-7	159	120	-3	103*	74	8	601	602	8	295	305	-2	479	495	-2	816	826
-6	848	864	-2	1075	993	9	79*	56	9	296	278	-1	506	524	-1	46*	40
-5	1302	1320	-1	233	230	H-8	H-8	3	6	492	491	0	582	575	0	582	575
-4	1283	1292	0	707	671	-5	145	121	-10	111*	56	-10	126*	32	-7	161	154
-3	1931	1935	1	398	403	-4	511	530	-9	743	739	-9	743	739	-6	230	227
-2	1621	1687	2	616	604	-3	473	464	-8	840	835	-8	840	835	-5	266	270
-1	1197	1141	3	939	926	-2	402	426	-7	556	583	-7	556	583	-4	266	270
0	383	355	4	1237	1177	-1	373	407	-6	409	433	-3	409	433	-3	409	433
1	1154	1130	5	147	126	0	127*	86	-5	379	419	-4	479	495	-2	416	416
2	699	673	6	153	139	1	101*	69	-4	399	435	-3	479	495	-2	416	416
3	93*	29	7	167	139	2	684	711	-3	518	507	-2	479	495	-1	360	371
4	1205	1126	H 6	2	2	3	651	636	-2	523	516	-1	392	340	6	360	371
5	641	610	-10	461	458	4	660	659	-1	262	257	-1	392	340	H-10	4	4
6	124*	93	-9	27*	34	5	57*	86	0	921	960	0	569	547	-2	161	172
7	277	281	-8	478	507	6	924	904	-1	124	112	1	948	913	-1	101*	116
8	315	313	-7	253	245	7	898	930	-2	364	376	2	304	295	0	281	301
9	202	146	-6	464	470	8	133	106	-3	490	476	3	304	295	0	357	322
10	601	598	-5	464	470	9	267	241	-2	490	476	4	146	90	1	357	322
H 1	2	2	-4	450	460	10	27*	24	-1	848	848	5	146	90	2	319	322
-11	48*	84	-3	546	538	H-7	H-7	3	0	1379	1379	6	102*	105	3	273	262
-10	115*	89	-2	464	436	-6	752	761	4	204	223	7	566	584	4	118*	142
-9	652	622	-1	464	436	-5	85*	55	5	510	503	8	450	449	5	614	592
-8	158	137	0	270	309	-4	824*	74	6	459	449	8	450	449	6	94*	94
-7	156	128	1	148	144	-3	124*	149	7	30*	25	7	30*	25	7	94*	94
-6	65*	51	2	110*	51	-4	124*	149	7	30*	25	8	450	449	8	94*	94







Fingerprint after Cycle 26

FACTOR = 10.00

H	DBS	CALC	H	DBS	CALC	H	DBS	CALC	H	DBS	CALC	H	DBS	CALC	H	DBS	CALC			
-8	115	71	-9	305	290	-7	188	240	5	452	445	-8	174	182	-7	277	255	-9	707	684
-7	1895	1918	-8	219	190	-6	117	11	5	129	81	-7	143	114	-6	114*	17	-8	93*	90
-6	166	181	-7	121	136	-5	187	181	5	374	385	-6	107*	90	-5	353	386	-7	770	764
-5	442	484	-6	63*	56	-4	165	155	8	264	250	-5	571	570	-4	752	746	-6	195	165
-4	396	391	-5	150	126	-3	28*	30	9	112*	100	-4	526	526	-3	1272	1252	-5	431	443
-3	573	568	-4	474	475	-2	28*	29	5	108*	147	-3	176	161	-2	363	371	-4	137	148
-2	1235	1189	-3	96*	70	-1	111*	71	5	108*	147	-1	176	161	-1	97*	125	-3	152	89
-1	441	443	-2	120	104	0	30*	66	5	1100	1089	0	163	149	0	776	748	-2	200	221
0	880	791	-1	358	357	1	637	632	5	206	207	-1	163	149	1	257	241	-1	349	360
1	155	128	0	374	357	2	305	300	5	206	203	-1	163	149	2	334	321	0	508	489
2	306	313	1	188	158	3	78*	33	8	129	81	-1	243	238	3	171	175	1	474	428
3	1036	997	2	510	590	4	30*	86	9	65*	63	-2	457	463	4	484	463	2	272	276
4	145	54	3	545	578	5	660	642	10	1078	1047	-2	182	170	5	484	513	3	103*	24
5	178	173	4	348	343	6	473	462	5	1394	1320	-2	108*	28	6	433	430	4	708	719
6	45*	632	5	215	230	7	580	570	6	481	468	-1	207	206	7	433	430	5	135	208
7	637	632	H	7	4	8	206	196	6	481	468	9	148	145	8	433	430	6	604	629
8	358	351	H	7	4	9	29*	94	7	1109	1120	9	148	145	9	433	430	7	708	719
9	199	216	H	7	4	10	137	193	8	532	515	9	148	145	9	433	430	8	708	719
H	1	4	H	7	4	H	-5	5	8	275	256	H	7	5	H	-4	6	H	2	6
-10	565	550	-8	115*	127	-8	725	692	5	275	256	-7	591	589	-8	430	404	-9	138	134
-9	26*	81	-5	24*	3	-7	381	378	5	60*	56	-6	561	564	-7	18*	1	-8	620	629
-8	116	105	-4	183	182	-6	102	47	5	75*	72	-5	185	189	-6	226	258	-7	229	214
-7	108*	123	-3	495	483	-5	237	238	6	833	818	-4	207	224	-5	227	198	-6	455	443
-6	281	261	-2	283	293	-4	152	84	7	809	792	-3	477	495	-4	30*	61	-5	337	310
-5	800	822	-1	271	264	-3	712	725	8	147	136	-2	28*	344	-3	128	120	-4	560	540
-4	872	881	0	510	542	-2	244	253	9	147	136	-1	28*	344	-2	234	240	-3	845	805
-3	610	592	1	302	309	-1	924	948	10	1100	1089	0	197	195	-1	1575	1516	-2	258	232
-2	597	563	2	58*	11	0	1112	1085	1	1100	1089	0	197	195	-1	1575	1516	-1	849	839
-1	250	243	3	417	417	1	585	578	2	747	727	1	311	339	0	345	341	0	291	305
0	581	586	H	8	4	2	53*	534	3	747	727	1	311	339	0	345	341	1	849	839
1	1178	1132	H	8	4	3	53*	534	4	816	821	2	569	586	1	773	768	2	291	305
2	34*	15	H	8	4	4	137	129	5	816	821	2	569	586	2	1095	1038	3	291	305
3	315	308	-7	330	387	5	228	185	6	816	821	2	569	586	3	1095	1038	4	291	305
4	28*	36	-6	70*	104	6	544	570	7	816	821	2	569	586	4	1095	1038	5	291	305
5	477	489	-5	292	289	7	544	570	8	816	821	2	569	586	5	1095	1038	6	291	305
6	217	216	-4	357	357	8	635	646	9	816	821	2	569	586	6	1095	1038	7	291	305
7	61*	101	-3	518	548	9	367	376	10	816	821	2	569	586	7	1095	1038	8	291	305
8	379	385	-2	94*	88	10	206	221	11	816	821	2	569	586	8	1095	1038	9	291	305
9	284	285	-1	28*	23	0	206	221	12	816	821	2	569	586	9	1095	1038	10	291	305
H	2	4	0	473	461	H	-4	5	13	816	821	2	569	586	H	-3	6	H	3	6
-10	38*	67	-8	108*	63	-8	108*	63	14	816	821	2	569	586	-8	26*	10	-9	177	173
-9	230	240	-7	140	140	-7	140	140	15	816	821	2	569	586	-7	340	346	-8	222	212
-8	239	253	-6	1012	1017	-6	1012	1017	16	816	821	2	569	586	-6	134	143	-7	455	443
-7	194	182	-5	429	406	-5	429	406	17	816	821	2	569	586	-5	30*	99	-6	237	231
-6	346	339	-4	136	120	-4	136	120	18	816	821	2	569	586	-4	28*	19	-5	499	509
-5	931	948	-3	636	650	-3	636	650	19	816	821	2	569	586	-3	28*	19	-4	548	536
-4	106*	30	-2	140	112	-2	140	112	20	816	821	2	569	586	-2	28*	19	-3	591	591
-3	464	465	-1	450	452	-1	450	452	21	816	821	2	569	586	-1	28*	19	-2	350	343
H	2	4	0	224	223	0	224	223	22	816	821	2	569	586	0	224	223	-1	350	343



6	215	225	348	384	515	513	144	136	236	283	330	326	412	417	
7	27*	97	167	206	126	76	374	339	299	275	692	705	412	417	
8	146	219	452	481	H-3	5	328	336	1 44*	78	88*	25	H 4	6	
H	3	4	386	392			1 251	251	127	82			H 4	6	
-10	286	302	29*	110	-9	137	687	688	3 585	575	H-2	6	-9	138	19
-9	160	153	153	105	-8	264	273	237	4 366	342	29*	8	-8	41*	24
-8	404	384	449	20	-7	416	29*	91	5 154	103	449	435	-7	299	291
-7	218	283	166	129	-6	783	798	185	6 377	379	129	139	-6	1099	1092
-6	29*	11	180	154	-5	899	904	381	7 936	913	82*	22	-5	347	354
-5	288	306	180		-4	296	904	186	8 39*	22	103*	26	-4	497	483
-4	577	586			-3	308	904	186	H-8	6	76*	84	-3	367	367
-3	1685	1641	H-9	5	-2	599	620		-4	76*	84		-2	185	219
-2	842	834	28*	26	-1	1043	1001		-3	676	667		-1	702	678
-1	753	737	396	396	0	97*	93	29	-2	29*	77		0	377	362
0	180	163	70*	79	1	222	206	206	-4	127	71		1	155	160
1	42*	114	27*	25	2	450	460	241	-3	464	441		2	135	178
2	489	676	324	309	3	983	973	192	-2	133	150		3	257	250
3	166	198	0	281	4	436	434	515	-1	119*	148		4	804	864
4	50*	21	256	281	5	539	537	310	0	115	77		5	182	179
5	186	185	507	498	6	109*	105	68	1	733	721		H 5	6	
6	427	432	41*	28	7	235	242	363	2	243	181		-8	26*	45
7	569	564	140	109	8	156	114	204	3	411	169		-7	217	297
H	4	4	501	511	9	426	461	388	4	299	294		-6	290	285
-10	95*	49	142	98	10	181	136	408	5	252	252		-5	310	309
-9	400	385	H-8	5	H-2	5	290	300	6	349	322		-4	690	689
-8	79*	83	126*	14	-9	358	342	727	-8	213	195		-3	999	1014
-7	30*	112	43*	47	-7	101*	96	266	-7	129	139		-2	37*	17
-6	487	492	52*	286	-6	28*	26	274	-6	440	462		-1	301	292
-5	344	322	43*	285	-5	323	336		-5	804	792		0	679	700
-4	438	413	272	377	-4	1139	1132		-4	579	587		2	72*	24
-3	634	614	376	381	-3	231	233		-3	362	376		3	385	424
-2	863	841	0	582	-2	790	776		-2	406	399		4	411	405
-1	536	531	378	381	-1	158	112		-1	347	323		H 6	6	
0	29*	20	31*	208	0	718	693		0	29*	30		-7	180	152
1	2R*	11	210	208	1	951	893		1	281	276		-6	160	175
2	842	821	684	659	2	490	502		2	829	813		-5	27*	58
3	241	249	502	493	3	715	712		3	475	470		-4	25*	22
4	115	110	270	268	4	196	194		4	159	157		-3	43*	36
5	645	659	455	443	5	378	368		5	388	373		-2	25*	28
6	565	560	98*	92	6	495	527		6	461	463		-1	194	188
7	103*	85	386	384	7	98*	34		7	207	252		0	501	528
H	5	4	H-7	5	8	63*	21		8	260	273		1	545	553
-10	274	273	27*	67	9	252	245		9	501	507		2	181	157
-9	97*	142	27*	324	H-1	5	499	501	H-6	6	277		H 7	6	
-8	496	501	219	211	-10	530	484	269	-7	278	298		-6	28*	24
-7	259	256	332	378	-9	423	392	82	-6	412	442		-5	180	194
-6	30*	31	332	378	-8	118	42	211	-5	120	18		-4	213	191
-5	365	361	179	240	-7	115*	101		-4	246	264		-3	226	216
-4	242	237	56*	70	-6	214	218		-3	392	401		-2	837	852
-3	403	411	30*	23	-5	115	140		-2	304	308		-1	502	502
-2	113*	90	642	634	-4	120	95		0	514	494		0	220	225
-1	1524	1482	416	395	-3	665	668		1	307	300		H-10	7	
0	479	471	192	169	-2	243	231		2	307	300		-1	121*	106
1	615	600	30*	127	-1	587	594		3	21*	48		0	220	225
2	765	766	25*	263	0	284	274		4	188	202		-1	121*	106
3	89*	44	25*	18	1	1132	1095		5	377	366		0	220	225
4	635	642	25*	18	2	444	446		6	307	325		1	142	43
5	324	310	707	722	3	79*	46		7	357	332		2	26*	78
6	243	284			4	462	460		8	28*	15				

Fingerite after Cycle 26

FACTOR = 10.00

H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	
3	72*	33	-8	378	362	1	472	476	0	109*	67	-5	344	366	5	26*	112	
4	761	725	-7	594	573	2	125	47	1	641	630	-4	94*	126	H	0	9	
5	143	81	-6	591	585	3	333	332	2	63*	14	-3	385	417	-3	291	313	
6	97*	113	-5	109*	129	4	429	449	3	637	647	-2	402	443	-2	99*	92	
H	-9	7	-4	159	154	H	5	7	4	432	439	-1	216	209	-7	455	420	
-3	276	288	-3	527	526	5	366	352	5	548	562	0	29*	79	-6	88*	159	
-2	688	703	-2	394	408	6	247	27	6	241	247	-5	224	227	-5	224	227	
-1	248	245	-1	480	457	7	263	261	7	263	261	-4	545	549	-4	545	549	
0	630	652	0	173	154	-7	336	27	H	-2	8	-3	24*	12	-3	24*	12	
1	544	546	1	496	489	-6	128	159	-2	422	384	-2	101*	76	-2	101*	76	
2	119*	78	2	473	471	-5	144	159	-1	226	208	-1	178	208	-1	178	208	
3	553	532	3	66*	669	-4	83*	361	0	519	455	0	522	533	0	522	533	
4	133	156	4	174	156	-3	319	322	1	27*	35	1	759	762	1	759	762	
5	161	185	5	543	568	-2	116	92	2	321	323	2	269	285	2	269	285	
6	304	289	6	453	434	-1	83*	111	3	254	280	3	28*	100	3	28*	100	
7	368	375	7	500	505	0	64*	117	4	29*	48	4	93*	100	4	93*	100	
H	-8	7	H	-1	7	H	6	7	5	124	141	5	88*	92	5	88*	92	
-4	112*	147	-9	186	183	-5	177	184	-1	689	689	-2	192	168	0	192	168	
-3	457	460	-8	26*	43	-4	179	182	0	165	168	-1	271	302	1	271	302	
-2	66*	78	-7	495	477	-3	83*	76	1	622	595	-4	163	139	2	324	306	
-1	758	770	-6	863	851	-2	348	366	2	177	182	-3	909	894	3	446	474	
0	1124	1082	-5	130	57	-1	57*	55	3	692	689	-2	124*	128	-5	518	513	
1	134	137	-4	753	715	0	112*	77	4	424	426	-1	278	300	-4	312	322	
2	511	510	-3	185	198	H	-9	8	5	125	128	-3	75*	36	-3	128	124	
3	199	158	-2	234	241	0	122	87	6	190	176	1	50*	40	-2	446	436	
4	27*	80	-1	270	332	-2	240	204	7	103*	40	2	710	710	-1	300	309	
5	196	181	0	691	686	-1	240	204	H	-1	8	3	52*	30	0	141	131	
6	515	501	1	366	334	0	31*	29	-9	175	164	4	121	77	1	142	131	
7	160	148	2	478	481	1	203	219	-7	81*	46	5	559	519	2	231	224	
8	165	113	3	512	544	2	112*	376	-6	98*	82	6	59	77	3	93*	30	
H	-7	7	4	586	125	3	406	376	-5	138	79	H	-6	9	H	2	9	
-5	160	169	5	95*	98	4	406	376	-4	29*	45	-5	146	129	-6	173	175	
-4	271	326	6	27*	11	5	731	737	-4	500	501	-4	81*	56	-5	307	315	
-3	260	265	7	81*	41	6	228	239	-3	1013	1007	-3	123	96	-4	143	82	
-2	104*	59	8	93*	125	H	-8	8	-2	20*	5	-2	272	282	-3	216	236	
-1	155	193	9	92*	39	H	0	7	0	768	791	-1	446	445	-2	651	657	
0	388	360	-9	341	324	0	214	205	1	1013	1007	0	627	604	-1	148	127	
3	137	94	-8	223	178	-2	189	163	2	125	258	1	229	253	0	355	362	
4	327	328	-7	26*	41	-1	304	271	3	279	182	2	151	153	1	141	161	
5	253	232	-6	1076	1022	0	319	335	4	310	299	3	284	263	2	453	466	
6	451	455	-5	570	569	1	529	519	5	27*	26	4	568	595	3	319	346	
7	94*	51	-4	28*	19	2	56*	85	6	H	0	H	-5	9	H	3	9	
8	762	766	-3	210	193	3	572	547	-8	263*	118	-5	115*	126	-5	712	709	
H	-6	7	-2	232	248	4	982	970	-7	367	342	-7	100*	62	-4	126	66	
-6	219	214	-1	931	893	5	180	160	-6	76*	27	-4	86*	66	-3	700	698	
-5	550	553	0	931	893	6	180	160	-5	93*	124	-3	86*	66	-2	293	275	
-4	225	218	1	343	318	7	370	399	-4	542	547	-2	122	93	-1	423	445	
			2	855	855	H	-7	8	-3	71*	139	-1	378	367	0	423	445	
			3	303	295				-2	123	120	0	250	276	1	122*	107	
			4	398	395										H	-2	11	



